

Assignment 3.

→ Show that isotropic material have only two independent Elastic Moduli.

Sol<sup>n</sup>:- We know

$$\sigma_{ij} = C_{ijkl} \epsilon_{kl}$$

where  $C_{ijkl}$  is stiffness and it has 81 components in  $9 \times 9$  Matrix notation.

\* But from, homogeneous Eq<sup>n</sup> of body

$$\sigma_{ij} = \sigma_{ji} \quad \&$$

also  $E_{ij} = E_{ji}$  (Symmetric matrix)

$$\text{So, } [C_{ijkl} = C_{jikl} = C_{ijlk}]$$

using it no. of independent component becomes 36.

\* & Strain energy ( $\psi$ ) is a scalar function

Elastic work done

$$d\psi = \sigma_{ij} d\epsilon_{ij} = C_{ijkl} \epsilon_{kl} d\epsilon_{ij}$$

$$\therefore \frac{d\psi}{d\epsilon_{ij}} = C_{ijkl} \epsilon_{kl} = \sigma_{ij}$$

$$\text{or } \frac{\partial}{\partial \epsilon_{kl}} \left[ \frac{d\psi}{d\epsilon_{ij}} \right] = C_{ijkl}$$

$$\text{or } \frac{d^2\psi}{\partial \epsilon_{kl} \partial \epsilon_{ij}} = C_{ijkl} = \frac{\partial}{\partial \epsilon_{ij}} \left[ \frac{d\psi}{d\epsilon_{kl}} \right] = C_{klij}$$

So,  $[C_{ikkl} = C_{kell}]$

It reduces no. of independent component from 36 to 21 only.

which can be written in Voigt's notation like:

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_4 \\ \sigma_5 \\ \sigma_6 \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & C_{14} & C_{15} & C_{16} \\ & C_{22} & C_{23} & C_{24} & C_{25} & C_{26} \\ & & C_{33} & C_{34} & C_{35} & C_{36} \\ & & & C_{44} & C_{45} & C_{46} \\ & & & & C_{55} & C_{56} \\ & & & & & C_{66} \end{bmatrix} \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \epsilon_3 \\ \epsilon_4 \\ \epsilon_5 \\ \epsilon_6 \end{bmatrix}$$

where

$$\sigma_1 = \sigma_{11}$$

$$\sigma_2 = \sigma_{22}$$

$$\sigma_3 = \sigma_{33}$$

$$\sigma_4 = \sigma_{23}$$

$$\sigma_5 = \sigma_{13}$$

$$\sigma_6 = \sigma_{12}$$

$$C_{11} = C_{1111}$$

$$C_{12} = C_{1122}$$

$$\dots$$

$$\dots$$

$$C_{34} = C_{3323}$$

So, on.

$$\epsilon_1 = \epsilon_{11}$$

$$\epsilon_2 = \epsilon_{22}$$

$$\epsilon_3 = \epsilon_{33}$$

$$\epsilon_4 = 2\epsilon_{23}$$

$$\epsilon_5 = 2\epsilon_{13}$$

$$\epsilon_6 = 2\epsilon_{12}$$

We know that isotropic material have identical property in all direction. So, any rotation from any axis will not change its property in that direction.

So, we are applying a 4-fold symmetry operation about z-axis. then there should be.

$$C'_{ijkl} = C_{pqrs}$$

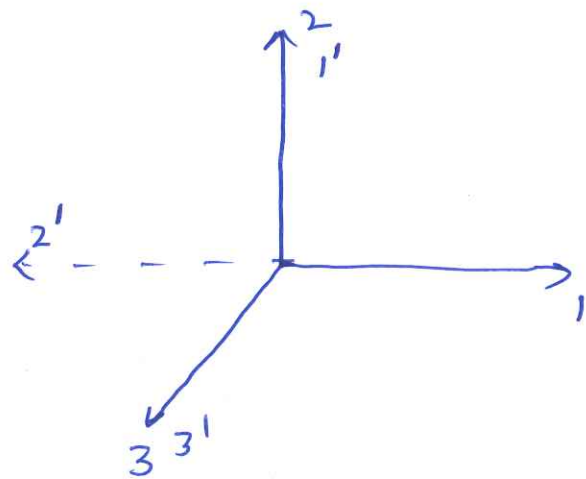
where  $C_{pqrs}$  is stiffness in old co-ordinate system.

&  $C'_{ijkl}$  is stiffness in new co-ordinate system.

in Voigt's notation it can be written as.

$$[C'_{mn} = C_{ab}]$$

$$A = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} = a_{ij}$$



for ~~the~~ transformation.

$$C'_{ijkl} = a_{ip} a_{jq} a_{kr} a_{ls} C_{pqrs}$$

It can be easily seen that after 4-fold rotation.

$1 \rightarrow 2$	or	$11 \rightarrow 22$	in Voigt's notation.	
$2 \rightarrow -1$		$22 \rightarrow (-1)(-1) \rightarrow 11$		$1 \rightarrow 2$
$3 \rightarrow 3$		$33 \rightarrow 33$		$2 \rightarrow 1$
		$23 \rightarrow -13$		$3 \rightarrow 3$
		$13 \rightarrow 23$		$4 \rightarrow -5$
		$12 \rightarrow -12$		$5 \rightarrow 4$
				$6 \rightarrow -6$

So, component of stiffness in new co-ordinate system can be written as: -

(1)  $C'_{11} \stackrel{\text{Transformation}}{=} C_{22} \stackrel{\text{Symmetry}}{=} C_{11}$

(2)  $C'_{12} = C_{21} = C_{12}$

(3)  $C'_{13} = C_{23} = C_{13}$

(4)  $C'_{14} = -C_{25} = C_{14}$

(5)  $C'_{15} = C_{24} = C_{15}$

(6)  $C'_{16} = -C_{26} = C_{16}$

(7)  $C'_{22} = C_{11} = C_{22}$

(8)  $C'_{23} = C_{13} = C_{23}$

(9)  $C'_{24} = -C_{15} = C_{24}$

(10)  $C'_{25} = C_{14} = C_{25}$

(11)  $C'_{26} = -C_{16} = C_{26}$

(12)  $C'_{33} = C_{33} = C_{33}$

(13)  $C'_{34} = -C_{35} = C_{34}$

(14)  $C'_{35} = C_{34} = C_{35}$

(15)  $C'_{36} = -C_{36} = C_{36}$

(16)  $C'_{44} = C_{55} = C_{44}$

(17)  $C'_{45} = -C_{54} = C_{45}$

(18)  $C'_{46} = C_{56} = C_{46}$

(19)  $C'_{55} = C_{44} = C_{55}$

(20)  $C'_{56} = -C_{46} = C_{56}$

(21)  $C'_{66} = C_{66} = C_{66}$

From (4) & (10)

$$C_{14} = -C_{25} = -C_{14} = 0$$

From (5) & (9)

$$C_{15} = C_{24} = -C_{15} = 0$$

From (13) & (14)

$$C_{34} = C_{35} = -C_{34} = 0$$

From (15)  $C_{36} = -C_{36} = 0$

From (17)

$$C_{45} = -C_{45} = 0$$

From (18) & (20)

$$C_{46} = C_{56} = -C_{46} = 0$$

From (1)

$$C_{11} = C_{22}$$

From (3)

$$C_{23} = C_{13}$$

From (19)

$$C_{44} = C_{55}$$

From (11)

$$C_{16} = -C_{26}$$

So, we have now 10 components becomes 'zero' and 4 components are related to others. The no. of independent component reduces from 21 to 7 only.

which can be written as.

$$G'_{ijkl} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & 0 & 0 & C_{16} \\ & C_{22} & C_{23} & 0 & 0 & C_{26} \\ & & C_{33} & 0 & 0 & 0 \\ & & & C_{44} & 0 & 0 \\ & & & & C_{55} & 0 \\ & & & & & C_{66} \end{bmatrix}$$

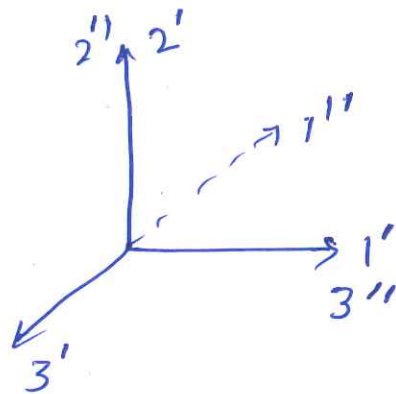
→ We are again applying 4-fold operation about Y-axis.

then  $C''_{ijkl} = C'_{pqrs} = C_{efgh}$

where  $C''_{ijkl}$  is new co-ordinate system after rotation about Y-axis.

or  $C''_{mn} = C'_{ab} = C_{efgh}$

$$A = [a_{ij}] = \begin{bmatrix} 0 & 0 & -1 \\ 0 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$



$$\& [C''_{ijkl} = a_{ip} a_{jq} a_{kr} a_{ls} C'_{pqrs}]$$

In Voigt's notation (rotation of  $90^\circ$  about  $y$ -axis)

$$\begin{array}{l}
 1 \rightarrow -3 \\
 2 \rightarrow 2 \\
 3 \rightarrow 1
 \end{array}
 \quad
 \left(
 \begin{array}{l}
 11 \rightarrow 33 \\
 22 \rightarrow 22 \\
 33 \rightarrow 11 \\
 23 \rightarrow 21 \\
 13 \rightarrow -31 \\
 12 \rightarrow -32
 \end{array}
 \right)
 \quad
 \left.
 \begin{array}{l}
 1 \rightarrow 3 \\
 2 \rightarrow 2 \\
 3 \rightarrow 1 \\
 4 \rightarrow 6 \\
 5 \rightarrow -5 \\
 6 \rightarrow -4
 \end{array}
 \right\}$$

The component of stiffness in new co-ordinate system are :-

$$(22) \quad C''_{11} = C_{33} = C_{11}$$

$$(29) \quad C''_{33} = C_{11} = C_{33}$$

$$(23) \quad C''_{12} = C_{32} = C_{12}$$

$$(30) \quad C''_{44} = C_{66} = C_{44}$$

$$(24) \quad C''_{13} = C_{31} = C_{13}$$

$$(31) \quad C''_{55} = C_{55} = C_{55}$$

$$(25) \quad C''_{16} = -C_{34} = C_{16}$$

$$(32) \quad C''_{66} = C_{44} = C_{66}$$

$$(26) \quad C''_{22} = C_{22} = C_{22}$$

$$(27) \quad C''_{23} = C_{21} = C_{23}$$

$$(28) \quad C''_{26} = -C_{24} = C_{26}$$

From (25), (13) & 14

$$C_{16} = -C_{34} = 0$$

From (28), (5) & 9

$$C_{26} = -C_{24} = 0$$

From (1) & (22)

$$C_{11} = C_{22} = C_{33}$$

From (19) & (32)

$$C_{44} = C_{55} = C_{66}$$

From (23)

$$C_{32} = C_{12} = C_{23}$$

So, now No. of independent component reduces from 7 to only '3' and can be written as

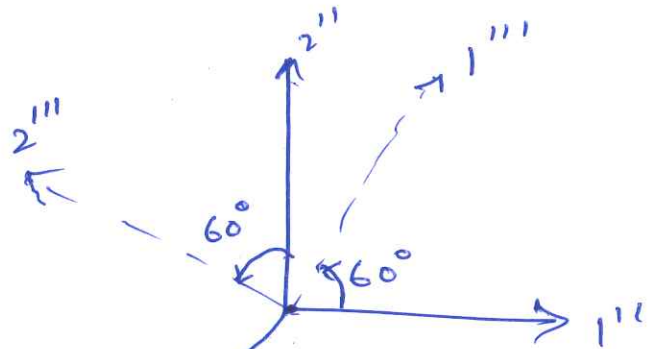
$$C''_{ijkl} = \begin{bmatrix} C_{11} & C_{12} & C_{12} & 0 & 0 & 0 \\ & C_{11} & C_{12} & 0 & 0 & 0 \\ & & C_{11} & 0 & 0 & 0 \\ & & & C_{44} & 0 & 0 \\ & & & & C_{44} & 0 \\ & & & & & C_{44} \end{bmatrix}$$

It expresses Cubical symmetry.

Since for isotropic material property will be same on any fold rotation. so Let's apply 6-fold rotation about Z-axis.

$$\& C'''_{ijkl} = C''_{pqrs}$$

$$\text{or } C'''_{mn} = C''_{ab}$$



$$A = [a_{ij}] = \begin{bmatrix} \cos 60 & \cos 30 & 0 \\ \cos 150 & \cos 60 & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 1/2 & \sqrt{3}/2 & 0 \\ -\sqrt{3}/2 & 1/2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$C'''_{ijkl} = a_{ip} a_{jq} a_{kr} a_{ls} C''_{pqrs}$$



In Voigt's notation transformation of axes after 6-fold rotation can be written as:-

From 'A' matrix.

$$1 \rightarrow \frac{1}{2}(1) + \frac{\sqrt{3}}{2}(2)$$

$$2 \rightarrow -\frac{\sqrt{3}}{2}(1) + \frac{1}{2}(2)$$

$$3 \rightarrow 3$$

where (1) (2) denote old co-ordinate axes.

Voigt's.  
So;

$$1 \rightarrow 11 \rightarrow \left( \frac{1}{2}(1) + \frac{\sqrt{3}}{2}(2) \right) \left( \frac{1}{2}(1) + \frac{\sqrt{3}}{2}(2) \right)$$

$$\rightarrow \frac{1}{4}(11) + \frac{\sqrt{3}}{2}(12) + \frac{3}{4}(22)$$

$$\rightarrow \frac{1}{4}(1) + \frac{\sqrt{3}}{2}(6) + \frac{3}{4}(2)$$

$$\text{i.e. } \left[ 1 \rightarrow \frac{1}{4}(1) + \frac{\sqrt{3}}{2}(6) + \frac{3}{4}(2) \right] \text{ --- (A)}$$

$$6 \rightarrow 12 \rightarrow \left( \frac{1}{2}(1) + \frac{\sqrt{3}}{2}(2) \right) \left( -\frac{\sqrt{3}}{2}(1) + \frac{1}{2}(2) \right)$$

$$\rightarrow -\frac{\sqrt{3}}{4}(11) - \frac{1}{2}(12) + \frac{\sqrt{3}}{4}(22)$$

$$\text{i.e. } \left[ 6 \rightarrow -\frac{\sqrt{3}}{4}(1) - \frac{1}{2}(6) + \frac{\sqrt{3}}{4}(2) \right] \text{ --- (B)}$$

$$4 \rightarrow 23 \rightarrow -\frac{\sqrt{3}}{2}(13) + \frac{1}{2}(23)$$

$$\text{or } \left[ 4 \rightarrow -\frac{\sqrt{3}}{2}(5) + \frac{1}{2}(4) \right] \text{ --- (C)}$$

Using (A) (B) (C) Voigt's notation transformation.

$$C_{11}''' = \left[ \frac{1}{4} (1) + \frac{\sqrt{3}}{2} (6) + \frac{3}{4} (2) \right] \left[ \frac{1}{4} (1) + \frac{\sqrt{3}}{2} (6) + \frac{3}{4} (2) \right] C$$

$$= \frac{1}{16} C_{11} + \left( \frac{\sqrt{3}}{8} + \frac{\sqrt{3}}{8} \right) C_{16} + \left( \frac{3}{16} + \frac{3}{16} \right) C_{12} + \frac{3}{4} C_{66} \\ + \left( \frac{3\sqrt{3}}{8} + \frac{3\sqrt{3}}{8} \right) C_{62} + \frac{9}{16} C_{22}$$

Symmetry.

$$\text{or } C_{11}''' \stackrel{\downarrow}{=} C_{11} = \frac{1}{16} C_{11} + \frac{\sqrt{3}}{4} C_{16} + \frac{3}{8} C_{12} + \frac{3}{4} C_{66} + \frac{3\sqrt{3}}{4} C_{62} \\ + \frac{9}{16} C_{22}$$

$$\& C_{16} = 0, C_{62} = 0 \quad \& C_{66} = C_{44}$$

$$\therefore C_{11} = \frac{1}{16} C_{11} + \frac{3}{8} C_{12} + \frac{3}{4} C_{44} + \frac{9}{16} C_{11}$$

$$\text{or } \frac{16}{16} C_{11} = \frac{10}{16} C_{11} + \frac{6}{16} C_{12} + \frac{12}{16} C_{44}$$

$$\text{or } \frac{6}{16} C_{11} = \frac{6}{16} C_{12} + \frac{12}{16} C_{44}$$

$$\text{or } \left[ C_{44} = \frac{C_{11} - C_{12}}{2} \right]$$

∴ No. of independent Component of Stiffness Matrix has reduces from '3' to '2' now, which can be written as, —

For Isotropic material:-

$$C_{ijkl} = \begin{bmatrix} C_{11} & C_{12} & C_{12} & 0 & 0 & 0 \\ & C_{11} & C_{12} & 0 & 0 & 0 \\ & & C_{11} & 0 & 0 & 0 \\ & & & \frac{C_{11}-C_{12}}{2} & 0 & 0 \\ & & & & \frac{C_{11}-C_{12}}{2} & 0 \\ & & & & & \frac{C_{11}-C_{12}}{2} \end{bmatrix}$$

The independent components are

$C_{11}$  &  $C_{12}$  only.

Proved